

# Study of Turbulence Structure with Atmospheric Stratification

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# Outline

- Introduction
- Turbulence structure under neutral stratification
- Analysis of anisotropy tensor
- Turbulence under uniform stratification and shear
- Summary and future work

# Introduction

- Risø has produced a model for the three-dimensional spectrum of turbulence,  $\Phi_{ij}$  (Mann,1994)
- Widely used in wind energy industry to simulate inflow turbulence for load calculations
- The Mann model incorporates Rapid Distortion Theory (RDT)
- Neutral surface layer
- Assumption of uniform mean shear
- Flat terrain and gently varying orography in neutral flow

The spectral velocity tensor;

$$\Phi_{ij}(\mathbf{k}) = \frac{1}{(2\pi)^3} \int R_{ij}(\mathbf{r}) \exp(-i\mathbf{k} \cdot \mathbf{r}) d\mathbf{r}, \quad (1)$$

where  $R_{ij}(\mathbf{r}) = \langle u_i(\mathbf{x}) u_j(\mathbf{x} + \mathbf{r}) \rangle$ , is the covariance tensor, and  $\langle \rangle$  denotes ensemble averaging.

$\Phi_{ij}(\mathbf{k})$  is modeled from the relation,

$$\frac{\langle dZ_i^*(\mathbf{k}(t), t) dZ_j(\mathbf{k}(t), t) \rangle}{dk_1 dk_2 dk_3} = \Phi_{ij}(\mathbf{k}(t), t), \quad (2)$$

where,  $u_i = \int e^{i\mathbf{k} \cdot \mathbf{x}} dZ_i(\mathbf{k}, t)$  (Fourier-Stieltjes integral)

# The RDT equation for neutral stratification

$$\frac{D}{Dt} dZ_i(\mathbf{k}, t) = \left( 2 \frac{k_i k_1}{k^2} - \delta_{i1} \right) \left( \frac{dU}{dz} \right) dZ_3(\mathbf{k}, t), \quad (3)$$

- The Mann spectral velocity tensor model contains only three adjustable parameters, determined from the one point measurements
- viz.,  $L, \Gamma$  and  $\alpha \epsilon^{2/3}$ , where the empirical value of  $\alpha \approx 1.7$

# Analysis of anisotropy tensor

Anisotropy stress tensor ;

$$b_{ij} = \frac{R_{ij}}{2k} - \frac{1}{3}\delta_{ij}, \quad (4)$$

where,  $k = \frac{1}{2}R_{ii}$ , is turbulent kinetic energy,  $R_{ij} = \langle u_i u_j \rangle$ , is the Reynolds stress tensor.

The three principal invariants are;

$$I_b = b_{ii} (= 0) \quad (5)$$

$$II_b = \frac{1}{2} [(b_{ii})^2 - b_{ii}^2] \quad (6)$$

$$III_b = \frac{1}{6} (b_{ii})^3 - \frac{1}{2} b_{ii} b_{jj}^2 + \frac{1}{3} b_{ii}^3 = \det(\mathbf{b}), \quad (7)$$

OR..

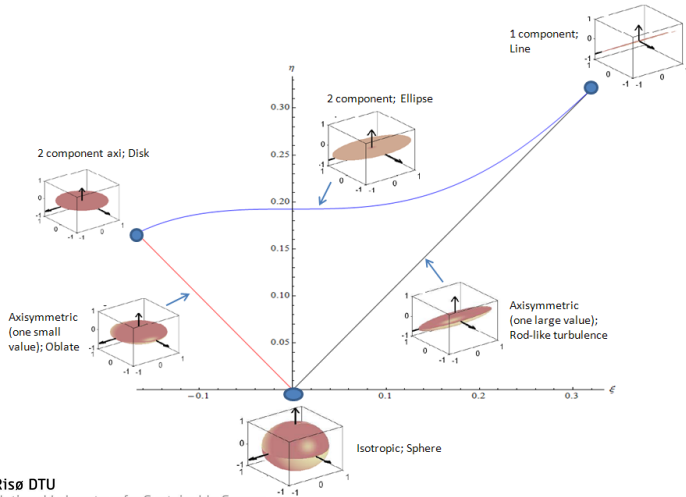
$$6\eta^2 = -2II_b = b_{ii}^2 = b_{ij}b_{ji} \quad (8)$$

$$6\xi^3 = 3III_b = b_{ii}^3 = b_{ij}b_{jk}b_{ki} \quad (9)$$

- Any point in the  $\xi - \eta$  plane represents the state of anisotropy of the Reynolds stresses that can occur at any point and time in any turbulent flow
- In the Mann model,  $b_{ij}$  becomes only function of the  $\Gamma$  parameter

# The Lumley triangle

( Source: A.J. Simonsen and P.-A. Krogstad, *Turbulent Stress Invariant Analysis: Clarification of Existing Terminology* )



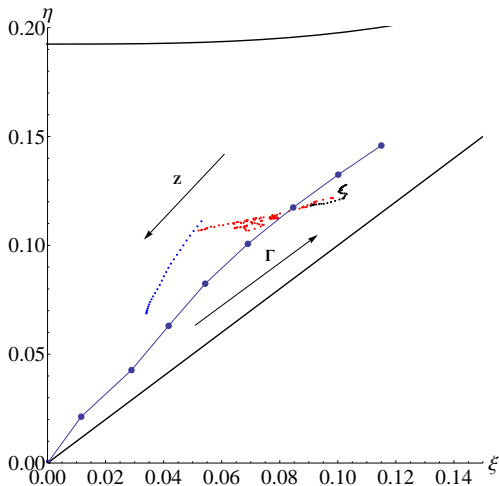


# NCAR LES data

	Stable	Neutral	Unstable
Domain [ $m^3$ ]	$1000 \times 1000 \times 400$	$2400 \times 2400 \times 1000$	$5120 \times 5120 \times 2048$
$\Delta x, \Delta y$ [ $m$ ]	2	4	10
$\Delta z$ [ $m$ ]	1	2.5	4
$z_i$ [ $m$ ]	188	616	1000
$\frac{z_i}{L}$	2	0	-10
$u_g$ [ $m/s$ ] ( $v_g = 0$ )	8	5	10
Number of $z$ levels [ $m$ ]	101	41	27

## LES data with Mann US model

.....; Neutral,.....; Stable,.....; Unstable, -●-; Mann US model



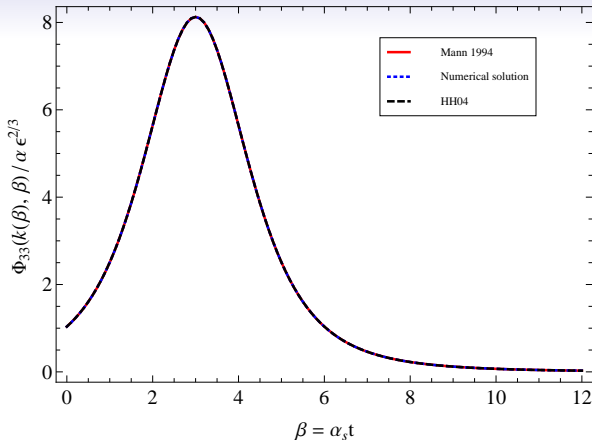
# Turbulence under uniform stratification and shear

The governing equations of RDT;

$$\begin{aligned} \frac{D}{Dt} dZ_i(\mathbf{k}, t) = & \left( 2 \frac{k_i k_1}{k^2} - \delta_{i1} \right) \left( \frac{dU}{dz} \right) dZ_3(\mathbf{k}, t) \\ & - \left( \frac{k_i k_3}{k^2} - \delta_{i3} \right) \frac{g}{T} d\Theta(\mathbf{k}, t), \end{aligned} \quad (10)$$

$$\frac{D}{Dt} d\Theta(\mathbf{k}, t) = -N^2 dZ_3(\mathbf{k}, t), \quad (11)$$

where,  $N^2 = (g/T)dT/dz$



$\Phi_{33}$  as function of  $\beta$  from numerical calculation in comparison with  $\Phi_{33}(k(\beta), \beta)$  from Mann (1994) and Hanazaki & Hunt (2004)

The initial, isotropic tensor is given as,

$$\Phi_{ij}(\mathbf{k}_0, 0) = \begin{bmatrix} \frac{k_2^2 + k_{30}^2}{4\pi k_0^4} & -\frac{k_1 k_2}{4\pi k_0^4} & -\frac{k_1 k_{30}}{4\pi k_0^4} & 0 \\ -\frac{k_1 k_2}{4\pi k_0^4} & \frac{k_1^2 + k_{30}^2}{4\pi k_0^4} & -\frac{k_2 k_{30}}{4\pi k_0^4} & 0 \\ -\frac{k_1 k_{30}}{4\pi k_0^4} & -\frac{k_2 k_{30}}{4\pi k_0^4} & \frac{k_1^2 + k_2^2}{4\pi k_0^4} & 0 \\ 0 & 0 & 0 & \frac{2\alpha_s^2 Ri}{4\pi k_0^2} \frac{S(k_0)}{E(k_0)} \end{bmatrix} \times E(k_0)$$

where,  $E(k_0)$  and  $S(k_0)$  are form of spectral densities such that initial kinetic energy,  $KE_0 = \int_0^\infty E(k_0) dk_0$  and initial potential energy,  $PE_0 = \int_0^\infty S(k_0) dk_0$  and  $k_0^4 = |\mathbf{k}_0|^4$ .

## Summary and Future work

- The analysis of the anisotropy tensor in the Lumley triangle represents a simple way of comparing stability dependant model
- The neutral case falls on/near  $\Gamma$  curve for  $\Gamma$  values ranging from 3 to 4
- The future task is to incorporate the eddy life time from the Mann spectral tensor model into the stability dependent RDT equations
- To solve and analyse numerically the spectra and co-spectra of all velocity components
- Comparisons with data will be made

**Thank you**