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Prediction of airfoil performance at high Reynolds numbers EFMC 2014, Copenhagen 17-20 Sept 2014

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Introduction Large Scale Wind Turbines

Increasing the rotor size may potentially lead to two obvious aerodynamic issues

- High Mach numbers in the tip region
 - Possible to avoid
 - Might be harmful for performance
- High Reynolds numbers
 - Hard to avoid
 - Might be beneficial for performance
 - Difficult to measure in controlled environment



DTU 10 MW Reference Turbine

Introduction Airfoil performance at high Reynolds Numbers



We expect that increasing the Reynolds Number will:

- Decrease the viscous effects due to the thinning of the boundary layer
- Promote earlier transition due to increased Reynolds number

Quantification the effects can be done by:

- Measurements
 - Tunnel measurements are difficult to obtain at high Re and low M
 - Openly available data are sparse
- Computations
 - Model performance in this range is unknown

Introduction Laminar turbulent transition

- The transition process depend on many parameters
 - Reynolds Number
 - Free stream turbulence level
 - Laminar separation bubbles
 - Cross flow
 - Surface roughness
 - Mass injection
- Typically approaches for transition modeling
 - *eⁿ* method (Orr-Sommerfeld eqn.)
 - Empirical correlations
 - Michel
 - Mayle
 - Abu-Ghannam and Shaw
 - Suzen



Introduction The $\gamma - Re_{\theta}$ Correlation based transition model

 The model is based on comparing the local Momentum Thickness Reynolds number with a critical value from empirical expressions

$$Re_{\theta} = Re_{\theta t}$$

 The following relation is used to simplify the computations in a general CFD code

$$\operatorname{Re}_{\theta} = rac{\operatorname{Re}_{\nu_t max}}{2.193}$$

- The model is based on transport equations, and can easily be implemented in general purpose flow solvers
- In the present form the model handles natural transition, by-pass transition, and separation induced transition
- The transition model is coupled to the k ω SST model through the production and destruction terms in the k-equation





Introduction *Eⁿ* model for natural transition

The E^n method is based on analyzing the behavior of small disturbances in the boundary layer

$$\psi(\mathbf{y}) = \phi(\mathbf{y}) \exp\left[i(\alpha \mathbf{x} - \omega t)\right]$$

The disturbances are inserted in the Navier-Stokes equations, and linearized to give the Orr-Sommerfeld equation

$$(U^* - \boldsymbol{c}^*)(\phi^{\prime\prime} - \alpha^2 \phi) - (u^*)^{\prime\prime} \phi = \frac{-i}{\alpha R \boldsymbol{e}_{\theta}}(\phi^{\prime\prime\prime\prime} - 2\alpha^2 \phi^{\prime\prime} + \alpha^4 \phi)$$

The Orr-Sommerfeld equation is solved with the following boundary conditions:

$$\phi(0) = \phi'(0) = 0$$
 and, $\phi(\infty) = \phi'(\infty) = 0$

In the EllipSys, the E^n model can be used together with a bypass and a bubble criteria.

Computational Setup Flow Solver

- We use the EllipSys2D incompressible solver.
- Diffusive terms by second order accurate central differences.
- Convective terms by QUICK.
- Steady state computations.
- Turbulence modeling by the $k \omega$ SST model
- Transitional computations using $\gamma Re_{\theta t}$ transition model and E^n model
- Reynolds number [3-40] million.

Test Cases Selected cases



- ♦ NACA63 018
- ◆ *DU*00 − *W* − 212
- NACA642A015

Test Case, NACA63-018 Computational setup

- Airfoil computations for Re=[3, 9, 20] million
- Using three transition models, E^n , E^n + BP and γRe_{θ}
- For natural transition we assume (N=9)
- Mesh resolution 384 × 256



Test Case, NACA63-018 Performance for varying Re





NACA63-018

The correlation based model do not respond correctly to varying Re !

Test Case, DU00-W-212 Computational set-up

- Airfoil computations for Re=[3, 9, 15] million
- Using three transition models, E^n , E^n + BP and γRe_{θ}
- All assuming natural transition (N=9)
- Mesh resolution 384 × 256



Test Case, DU00-W-212 Lift, Natural Transition



DU00-W-212, RE=3E6, N=9

Test Case, DU00-W-212 Lift, Natural Transition



DU00-W-212, RE=9E6, N=9

Test Case, DU00-W-212 Lift, Natural Transition



DU00-W-212, RE=15E6, N=9

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Test Case, DU00-W-212 Drag, Natural Transition



Test Case, DU00-W-212 Drag, Natural Transition





DU00-W-212, RE=9E6, N=9

Test Case, DU00-W-212 Drag, Natural Transition



DU00-W-212, RE=15E6, N=9

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Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=3E6, N=9

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Test Case, DU00-W-212 Transition Location, Natural Transition





DU00-W-212, RE=9E6, N=9

Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=15E6, N=9

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Test Case, NACA64₂A015 Computational setup

- Airfoil computations for Re=[10:40] million, AOA=0 deg.
- Using two transition models, E^n and γRe_{θ}
- Mesh resolution 384 × 256



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Test Case, NACA64₂A015 Performance at high Re



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Test Case, NACA64₂A015 Performance at high Re





Explanation

Behavior of the correlation based model

The following behavior is observed

- The Reynolds number is varied through the viscosity
- The pressure distribution stays nearly constant
- Turbulent quantities are unchanged away from the airfoil
- The critical Reynolds number predicted by the γRe_{θ} model stays constant



Conclusion Conclusion and outlook



We need further validation at high Re and relatively low Mach

- Wind turbine rotors will face high Re with increasing size
- Lift is weakly dependent on the transition location in normal operation even at high Re
- The available data show that the γRe_{θ} model over-predict drag at high Re
- Very little data available for comparison
- New data will be provided by the AVATAR project for the DU00-W-212 airfoil
- \blacklozenge The National Wind Tunnel could provide data Re \sim 10 Mill for low AOA